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## Compact Millimeter-Wave Switched-Beam Antenna Arrays for Short Range Communications

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# Compact Millimeter-Wave Switched-Beam Antenna Arrays for Short Range Communications

A. T. Alreshaid<sup>1</sup>, M. S. Sharawi<sup>1</sup>, S. Podilchak<sup>2</sup> and K. Sarabandi<sup>3</sup>

<sup>1</sup>Electrical Engineering Department, King Fahd University of Petroleum & Minerals, Dhahran, 31261, Saudia Arabia.

Email: [alreshaid@kfupm.edu.sa](mailto:alreshaid@kfupm.edu.sa) ; [msharawi@kfupm.edu.sa](mailto:msharawi@kfupm.edu.sa)

<sup>2</sup>Institute of Sensors, Signals and Systems within the School of Engineering and Physical Sciences at Heriot-Watt University, Edinburgh, Scotland, UK, EH14 4AS

Email: [s.podilchak@hw.ac.uk](mailto:s.podilchak@hw.ac.uk)

<sup>3</sup>Electrical and Computer Engineering Department, University of Michigan, Ann arbor, MI 48109 USA

Email: [saraband@umich.edu](mailto:saraband@umich.edu)

**Abstract**— The need for more data throughput is a requirement that will keep growing in future wireless standards, and during the past few years, millimeter-wave technology has generated much excitement in the mobile and wireless communications sectors due to the large bandwidth it can offer. In this letter two different travelling-wave, slot antenna arrays are proposed which can offer tunable switched-beam capability at millimeter-wave frequencies. The antenna systems are built on a single layer PCB with top- and bottom-side etching for operation at 28 GHz with at least 0.7 GHz of measured impedance bandwidth. For the first design, a planar 2x4 slot antenna array is proposed while the second design is implemented using a 4x4 slot array to demonstrate improved beam directivity. A Butler matrix for simple beam switching in the far-field is also integrated within the compact antenna structure to provide the needed phased array operation. The total size of the two proposed systems with their feed networks are 55.2 x 55 x 0.13 mm<sup>3</sup> and 53.7 x 61.2 x 0.13 mm<sup>3</sup>, respectively. These new travelling-wave switched beam arrays can be placed within current handheld mobile devices for high bandwidth short range communications enabling 5G technologies.

**Key Words**— Butler beam-forming network, millimeter-wave, slot antenna, switched beam, traveling-wave antenna, 5G.

## I. INTRODUCTION

The exponential increase in the volume of data traffic has motivated researchers to start exploring and nominating the millimeter-wave (mm-wave) spectrum as a candidate to provide channels with large bandwidths (BW) for fifth generation (5G) wireless communication systems. All wireless standards operating in the frequency range from 700

1 MHz to 2.6 GHz have limited channel BWs, thus limiting the amount of data for transmission. By up converting the  
2 communication frequency to 28 GHz or 38 GHz the allocated BW can increase significantly, providing data speeds  
3 much higher than what is provided by the latest technology launched to-date, more specifically, long-term-evolution  
4 advanced (LTE-A).  
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9 This immediate need for high data throughput at millimeter-wave frequencies can be met by utilizing robust radio  
10 access technologies. However, when considering frequency systems operating around 60 GHz, for example, high  
11 path loss due to atmospheric absorption can be observed. On the other hand, it was recently found that the attenuation  
12 caused by this phenomena at 28 GHz is only 0.012 dB over 200 m and 0.016 dB over the same distance at 38 GHz,  
13 thus providing a good frequency candidate for future wireless systems and enabling the possibility for high data rate  
14 throughputs with large BWs [1], [2]. Moreover, by taking advantage of the 28 GHz operational frequency, the  
15 corresponding wavelength is much smaller than more conventional communication schemes and thus mobile devices  
16 can support more antenna elements and arrays for higher gain. This can compensate for the free-space path losses  
17 introduced in the millimeter-wave communications channel.  
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25 The design of such 5G mobile terminals employing compact and tunable traveling-wave arrays with switched-  
26 beam capability, and other leaky-wave phased arrays [3] for wireless technologies at millimeter-wave frequencies,  
27 has not been widely investigated in the literature. There have been a few notable works at microwave frequencies  
28 where tunable series-fed patch antenna array elements, using new phased array approaches, have been demonstrated  
29 [4-6]. However, additional antenna research should be encouraged to meet the needs for beam controllable  
30 millimeter-wave antenna arrays enabling the aforementioned short-range communications. This is because with a  
31 limited number of radiating elements, compact series-fed antenna arrays can offer beam directivities on the order of  
32 10 dB with half-power beam widths which are typically less than 8°.  
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40 To enable pattern control for these types of traveling-wave antennas using simpler phased array approaches, beam-  
41 forming networks are needed for pattern switching and control in the far-field. The Butler network may be preferred  
42 for mobile communications since it is a relatively simple feeding structure with low-losses offering low-cost  
43 implementation and simple integration with hand-held terminals. Moreover, few works have concentrated on  
44 designing Butler networks at millimeter-wave frequency, such as [7] and [8] at 60 GHz, while the rest of the papers  
45 operated below 13 GHz such as [9] and [10]. In [11], for example, a 24 GHz Butler network was designed on silicon  
46 using 0.18  $\mu\text{m}$  CMOS technology with no antenna elements for radiation. It provided a BW of 2 GHz where the core  
47 Butler circuitry was only 0.9 mm by 0.46 mm, excluding the outer connections and the input/output ports. An  
48 integrated Butler with patches was designed in [11]. The operating frequency was 60 GHz providing a BW of 3 GHz.  
49 The system was built on an RT/duroid 5880 substrate with dielectric constant of 2.2 and thickness of 0.127 mm. The  
50 gain of the antennas was between 7 and 8.9 dBi. Most of the antennas for these systems were based on patches or  
51 quasi-yagi antennas in a linear array setup.  
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In this work, we propose two versions of one of the first traveling-wave antenna arrays using a Butler matrix for switched-beam diversity at 28 GHz. The proposed designs (see Fig. 1) are implemented using an array of series-fed slots printed on a single layer PCB with top- and bottom-side etching. To our knowledge this is the first time that such traveling-wave phased arrays with an integrated beam forming network have been designed, measured, and experimentally verified, while also, offering simple low cost implementation. The first version of the system contains a 2x4 slot antenna array integrated with its Butler feed network, while the second version is a similar 4x4 array. The measured -10 dB impedance BWs were at least 0.8 GHz and 0.7 GHz for the 2x4 and the 4x4 array, respectively. In addition, measured gain values for the two designs ranged from 5 to 7 dB and simulations and measurements are presented demonstrating good performance for the compact switched-beam travelling-wave antennas.

II. DESIGN DETAILS

There are several configurations of networks that can provide multi/switched beam control, such as the Butler matrix, the phased array network, and the Rotman and Bootlace lenses [12]. They can be classified into different categories; active and passive, steering and non-steering, simple and complex. Each configuration has its own advantages and disadvantages. Due to the Butler network's advantages over other types like its compact design, passive architecture, and the absence of external control, it has been selected to feed the proposed traveling-wave antenna arrays, mainly, to offer low cost, switched beam capability and simple integration with other electronic components.

In this letter, the Butler beam forming network is 4x4, so the insertion phases feeding the traveling-wave arrays are -135°, -45°, +45° and +135° respectively. This can offer beam steering at broadside for the angles -45°, -20°, +20° and +45° in a transverse plane perpendicular to the system board. More specifically, our 4x4 Butler network for millimeter-wave frequencies consists of 4 couplers, 2 crossovers, and 4 phase delay lines. These feed systems and antenna arrays are built on a thin (0.13mm) Rogers 3003 substrate with a dielectric constant of 3 to reduce surface wave excitation and improve radiation efficiency. According to these parameters, the width of the microstrip line is 0.33 mm to provide an impedance of 50-Ω. Also, the dimensions of the hybrid coupler arms are 0.19 mm by 2.44 mm for the thin arm (50-Ω) and 0.41mm by 2.2 mm for the thicker one (35.35-Ω). The crossover is achieved by cascading two of these hybrid couplers, which results in passing the two signals across each transmission line with the some loss and phase shift. Fig. 1 illustrates the layout of the two proposed antenna arrays while dimensions for their slot elements are described in Table I.

Table 1 Antenna Array Design Parameters for the two versions

Fig. 1 Layouts of Butler network integrated with a (a) 2x4 and a (b) 4x4 slot antenna array

For an ideal Butler network, the injected signal is divided equally between the output ports with an expected insertion loss of 6 dB at the output terminals. The challenge in the design is to minimize the losses and maintain the required phase difference between the output ports feeding the traveling-wave antenna arrays over a large operating bandwidth. In beam switching operation, one port is excited at a time, giving rise to one out of four beam directions. Other wideband designs have also been implemented and reported in the literature as recently reported in [13].

The slot antenna element is chosen in this work because of its easy implementation and simple integration within the ground plane. The designed slot antenna, which has a width of 0.4 mm, is fed by the 50- $\Omega$  microstrip feeding line. For the 2x4 structure, the slot's center is shifted by 1.3 mm from the center of the feeding line for 50- $\Omega$  matching. It has a length of half a wavelength, which has been optimized through simulations to 3.45 mm. The spacing between the centers of the adjacent slots is 6.9 mm. The proposed planar arrays utilize parallel feeding such that each microstrip feeding line excites a series array of slots defining a traveling-wave antenna. As a result, the overall size of the 2x4 and 4x4 antenna systems are 55.2 x 55 x 0.13 mm<sup>3</sup> and 53.7 x 61.2 x 0.13 mm<sup>3</sup>, respectively.

### III. RESULTS & DISCUSSIONS

The optimization and simulations of the design were performed using HFSS<sup>TM</sup>. Also, the phase delay lines within the feeding network were optimized to provide the required insertion phases at the input of the antenna arrays. Due to the use of mini-SMP connectors as external ports in the individual Butler design, as well as inputs in the complete system design, pads were placed around the ports with ground connected vias. The use of mini-SMP connectors also placed another restriction which was that the minimum distance between the input lines had to be greater than 5 mm [14]. This resulted in an increased separation of the input mini-SMP connectors from the Butler matrix feed system

When port 1 was excited, within the Butler matrix, the simulated power levels detected at the output ports varied from -10.4 to -6.1 dB while they varied from -9.3 to -7.6 dB for port 2. For the phases when port 1 was excited, the phase differences between the output ports was -51.5° between ports 5 and 6, -42.5° between ports 6 and 7, and -48.9° between ports 7 and 8. That introduces an average error of 4° from the ideal difference of -45°. For the second port, the differences were 144.4°, 133.4° and 122.74° which make an average phase shift of 7.7° from the ideal values of 135°. Tuning the network to obtain the required phase differences between the output ports was quite challenging. That was due to two main factors. The first one was to monitor the amplitude response and not to introduce more losses, while the second issue was the difficulty of tuning the phase differences between all the array input phases.

Fig. 2 shows the simulated reflection coefficient curves for all input ports for the 4x4 design as well as its port coupling. A slight shift in the desired resonance frequency is observed (i.e. now it is 29 GHz). Similar values were observed for the 2x4 antenna structure. The simulated 3D gain patterns for the complete millimeter-wave, switched beam traveling-wave antenna array are shown in Fig. 3. A maximum value of approximately 4.6dB was pointing at  $\theta = 45^\circ$  and  $135^\circ$  from the z-axis when port 1 was excited for the 4x4 array. When port 2 was excited, the beam went to

-20° and -160°, with 6.5dBi gain. Similar behavior was observed for the 2x4 design, with slightly lower gain values (4.1 and 6.4 dBi for ports 1 and 2, respectively). The other two ports behaved similarly.

**Fig. 2** Simulated port parameter curves for the 4x4 antenna array, (a) reflection coefficients, (b) port coupling.

**Fig. 2** Simulated 3D Gain pattern for the 4x4 antenna array integrated with Butler at 28.5 GHz when (a) port 1 or (b) port 2 is excited

Photographs of the fabricated prototypes are shown in Fig. 4 with front and back views. The responses experienced a frequency shift of approximately 1 GHz when comparing simulations against measurements due to the fabrication tolerances and possible material variations. In addition, the connector model was not incorporated into the simulations, only its pad. The measured input port S-parameters for the two designs are shown in Fig. 5 and were conducted at KFUPM, Saudi Arabia, using an Agilent PNA (N5572A). As can be noted from Fig. 5(a), port 1 of the 2x4 antenna array system has a BW of 720 MHz centered at 26.64 GHz and 800 MHz from 27.44 to 28.44 GHz. A one GHz BW is achieved by port 2 centered at 25.95 GHz. It also has a BW of 760 MHz centered at 27.7 GHz. It can be summarized that the 2x4 antenna array provided a BW of about 0.8 GHz centered around 27.8 GHz for all ports. For the 4x4 design, port 1 achieved a measured BW of 1.24 GHz centered at 28.3 GHz. The second port has 720 MHz centered at 27.9 GHz and 1.04 GHz at 26.1GHz. The overall BW of the 4x4 array is about 0.8 GHz centered at 28 GHz.

**Fig. 4** The top view of the fabricated models for the: (a) 2x4 and (b) 4x4 antenna array. Inset pictures show the back view of the antennas.

**Fig. 3** Measured reflection coefficients for (a) the 2x4 antenna array system (b) the 4x4 antenna array system

The radiation patterns for both designs were measured in the anechoic chamber facility at the Royal Military College of Canada, ON, Canada, and the University of Michigan, Ann Arbor, USA. Figs. 6(a) and (b) show the normalized measured patterns for the two arrays for their upper halves. The beams were successfully steered from broadside with peak gains ranging from 5 to 7 dBi. The 2x4 array had wider beamwidths for ports 2,3 compared to 1,4, while the 4x4 array had comparable beamwidths for all ports due to array symmetry.

**Fig. 6** Measured patterns at (a) 27.6 GHz for the 2x4 antenna system for all ports, (b) 27.8 GHz for the 4x4 antenna system for all ports (continuous line co-pol values, dashed-dotted line x-pol levels).



## IV. CONCLUSIONS

In this work, two versions (2x4 and 4x4) of millimeter-wave beam switching antenna arrays have been designed, fabricated and measured. The feeding network was based on a Butler matrix and slot elements were employed within the traveling-wave phased arrays. The overall antenna sizes were 55.2 mm by 55.0 mm by 0.13 mm and 53.7 mm by 61.2 mm by 0.13 mm, nominating them as suitable short-range solutions for handheld devices. The minimum measured BWs were 0.8 GHz and 0.7 GHz for the 2x4 and the 4x4 antenna structures, respectively, and both cover the 28 GHz band of operation. The peak gain for the antenna systems (feed network and arrays) ranged from 5 to 7 dB.

## ACKNOWLEDGEMENTS

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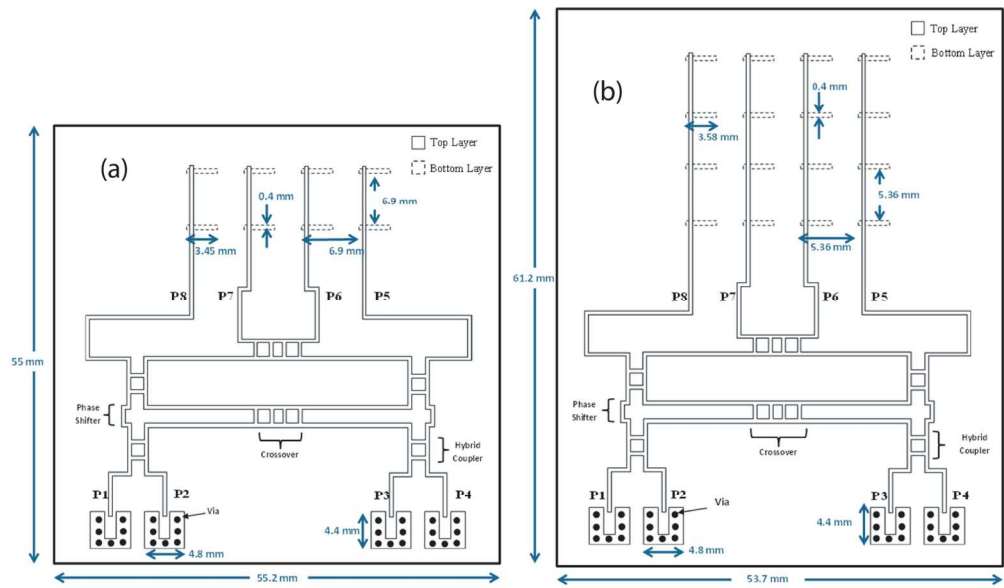


Fig1 Layouts of Butler network integrated with a (a) 2x4 and a (b) 4x4 slot antenna array 134x78mm (300 x 300 DPI)

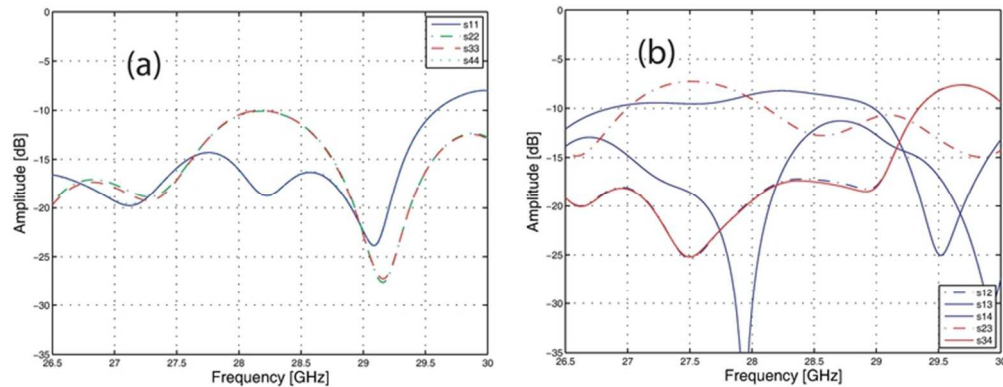


Fig 2 Simulated port parameter curves for the 4x4 antenna array, (a) reflection coefficients, (b) port coupling.  
70x27mm (300 x 300 DPI)

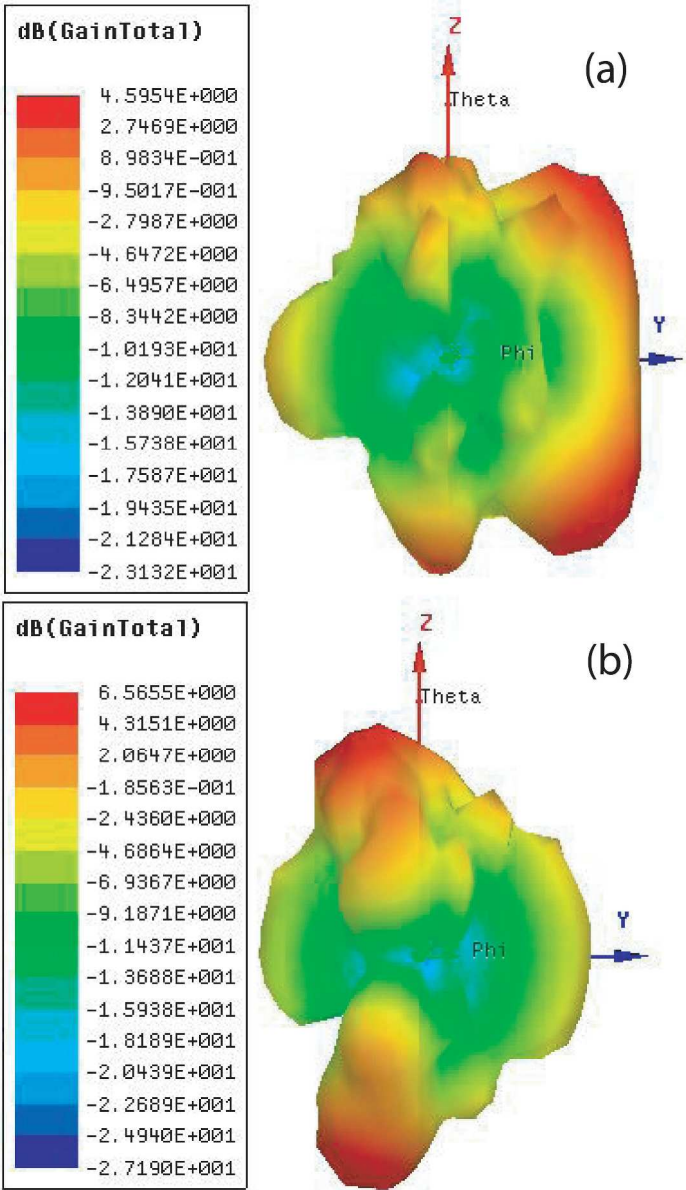


Fig3 Simulated 3D Gain pattern for the 4x4 antenna array integrated with Butler at 28.5 GHz when (a) port 1 or (b) port 2 is excited  
234x399mm (300 x 300 DPI)

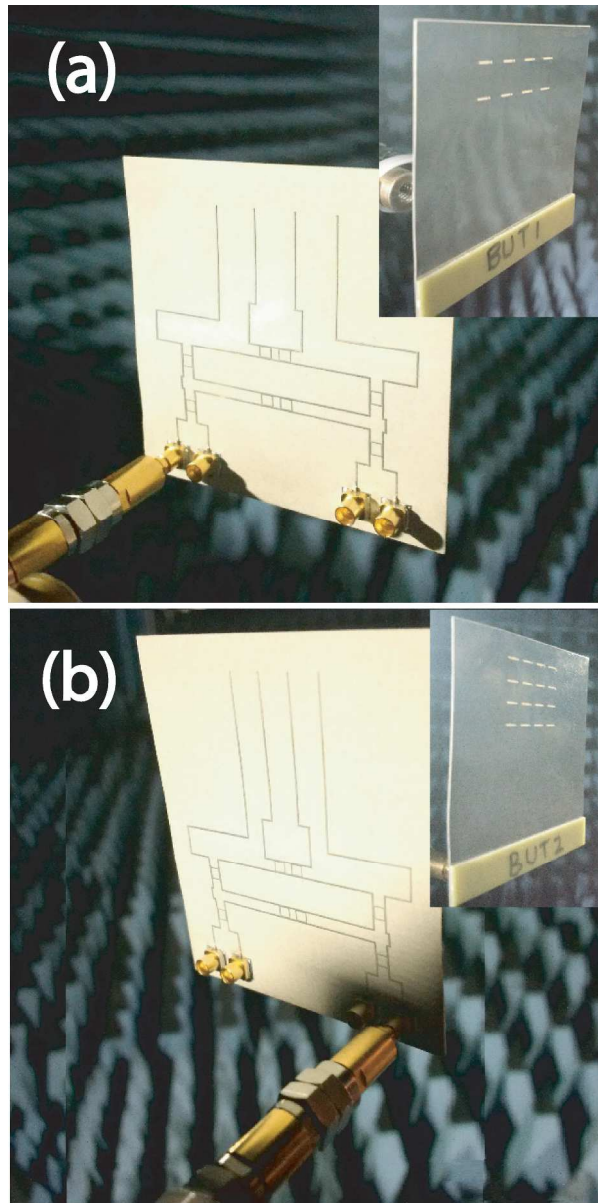
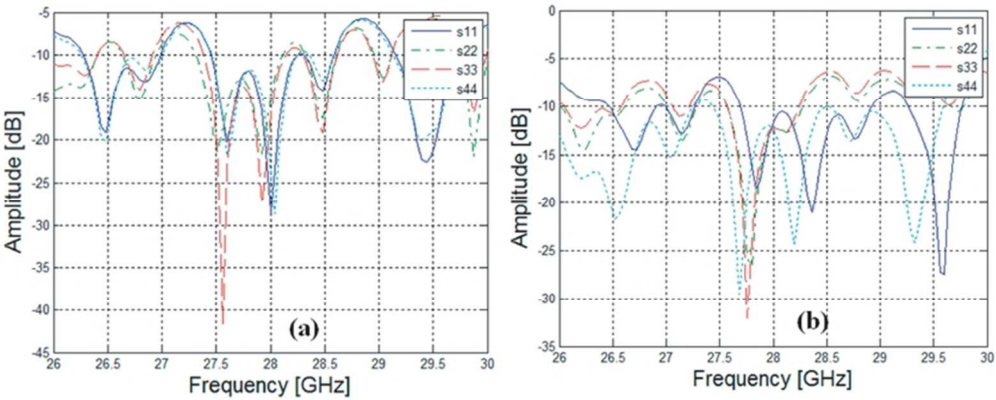


Fig 4 The top view of the fabricated models for the: (a) 2x4 and (b) 4x4 antenna array. Inset pictures show the back view of the antennas.  
216x434mm (300 x 300 DPI)



Fgi 5 Measured reflection coefficients for (a) the 2x4 antenna array system (b) the 4x4 antenna array system  
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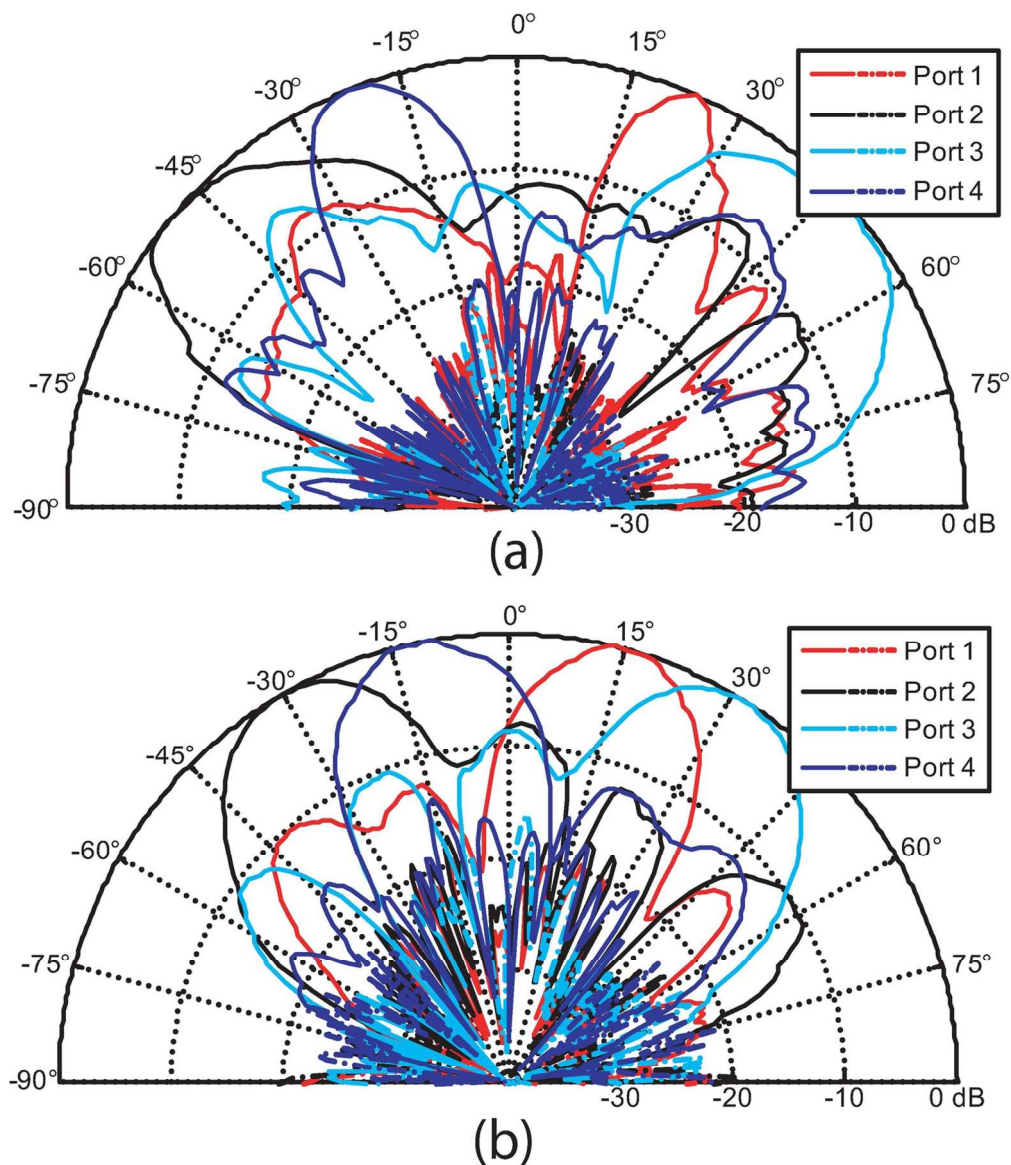


Fig 6 Measured patterns at (a) 27.6 GHz for the 2x4 antenna system for all ports, (b) 27.8 GHz for the 4x4 antenna system for all ports (continuous line co-pol values, dashed-dotted line x-pol levels).  
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For Peer Review

	<i>Slot's Width (mm)</i>	<i>Slot's Length (mm)</i>	<i>Horizontal Shift from feed's center (mm)</i>	<i>Inter-element Spacing (mm)</i>	<i># elements per feed (Series)</i>
<i>Version I</i>	0.4	3.45	1.3	6.9	2
<i>Version II</i>	0.4	3.58	1.36	5.36	4